

CONFIGURATION OF THE GFDL FV DYNAMICAL CORE

Lucas Harris
GFDL AM3 Summer School
17 July 2012


```
&fv_core_nml
```

```
  layout      = $fv_layout
```

```
  io_layout   = $fv_io_layout
```

```
  npx         = 49,
```

```
  npy         = 49,
```

```
  ntiles      = 6,
```

```
  npz         = 48,
```

```
  n_split     = 8,
```

```
  a2b_ord     = 4,
```

```
  adjust_dry_mass = $adjust_dry_mass,
```

```
  consv_te    = 0.7,
```

```
  fill        = .true.
```

```
  print_freq  = 0,
```

```
  grid_type   = 0,
```

```
  old_divg_damp = .true.,
```

```
  nord        = 0,
```

```
  dddmp       = 0.0,
```

```
  d2_bg       = 0.0075,
```

```
  d4_bg       = 0.00,
```

```
  tau         = 0.
```

```
/
```

```
&coupler_nml
```

```
...
```

```
  dt_atmos    = 1200
```

```
/
```

Discussed by
computing services

Model resolution

Time step

Damping

Dynamics

Diagnostics

Grid options

NAMELIST DEFAULTS

- A options which is not specified in `fv_core_nml` is assigned a default value (see `fv_arrays.F90` or `fv_control.F90` for more information)
- Some options **must** be specified:
 - `npx, npy, npz`
 - `ntiles = 6`
 - `layout`

WARNING

- If you don't know what an option does, don't mess with it
- Unfortunately no `do_what_I_want = .true. option`




```

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  npz         = 48,
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  adjust_dry_mass = $adjust_dry_mass,
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  print_freq  = 0,
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&coupler_nml
  ...
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```

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Model resolution

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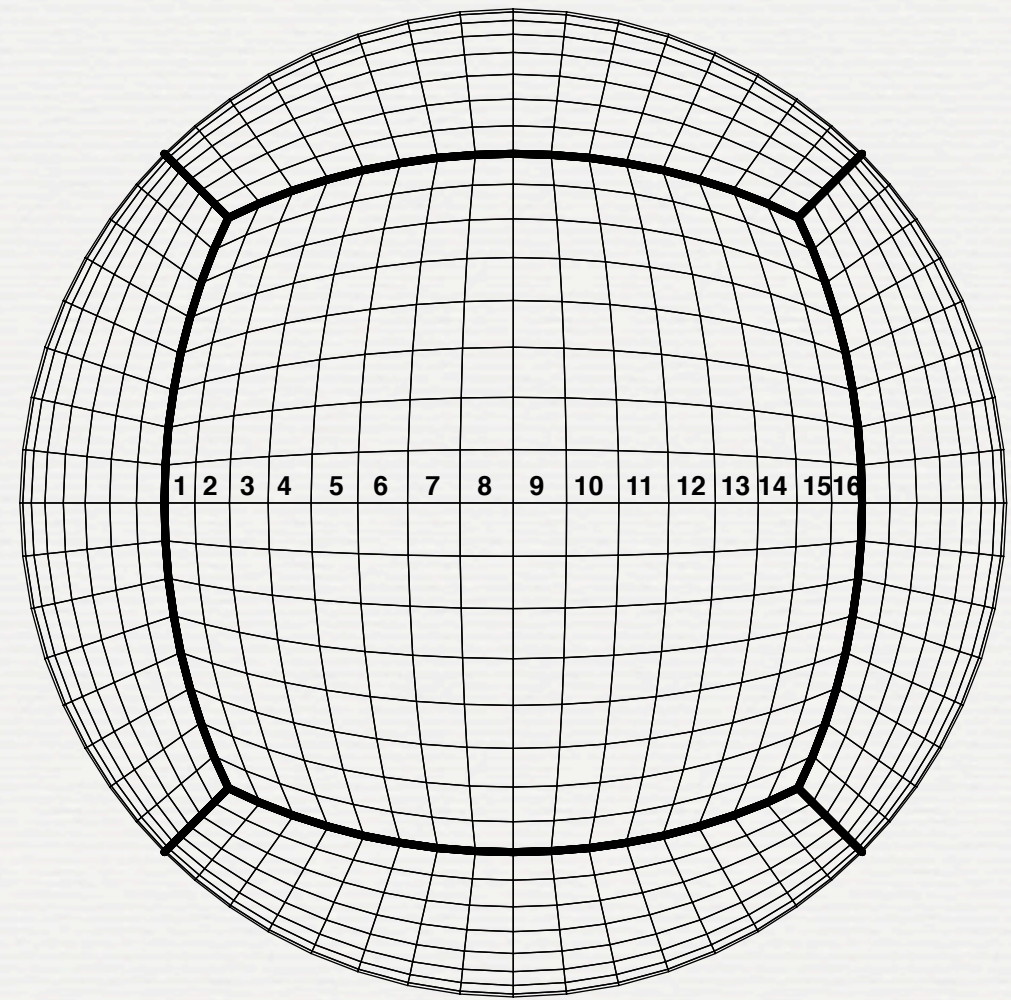
Dynamics

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MODEL RESOLUTION

- np_x, np_y : number of **grid corners** across a cube face
- $np_x - 1$ **grid cells** across a cube face
- np_x and np_y must be the same
- $np_x - 1$ and $np_y - 1$ ideally divisible by layout

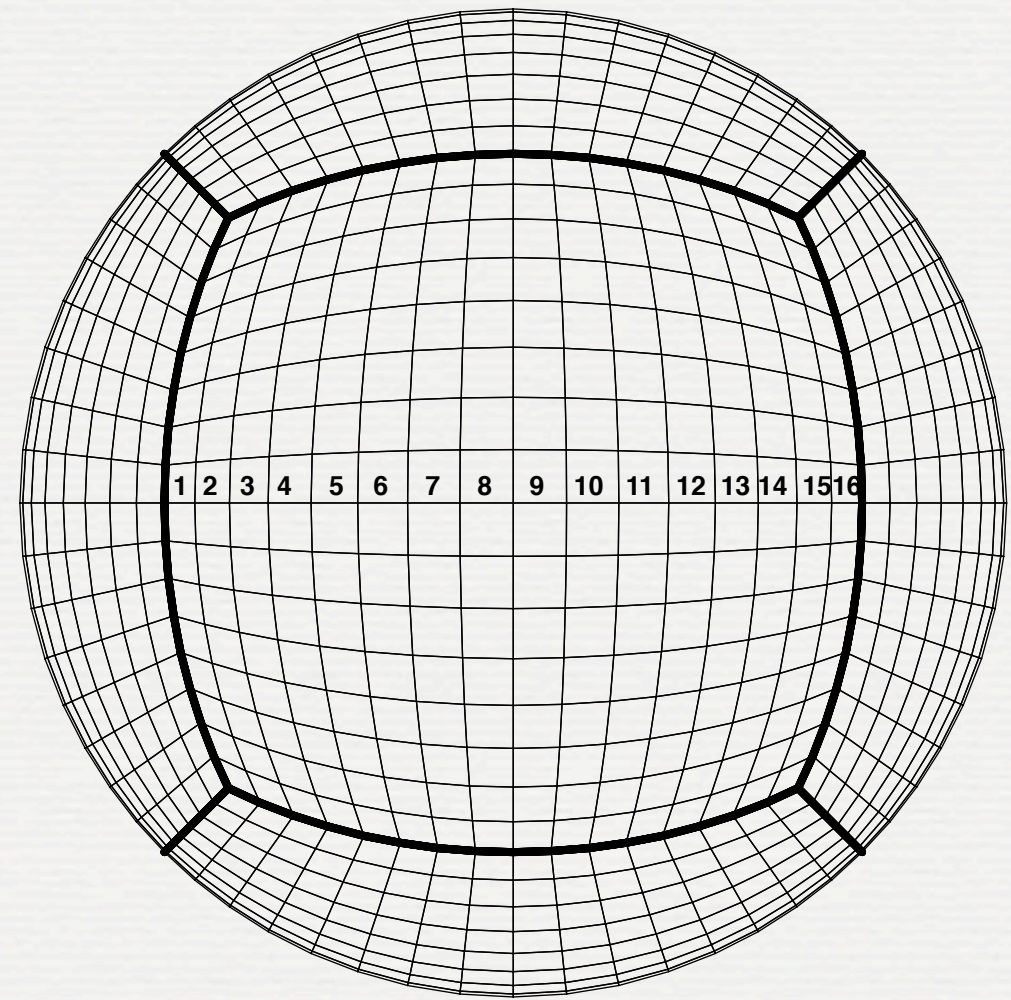


c16 grid

$$np_x = np_y = 17$$

MODEL RESOLUTION

- Average cell width of a cN grid is roughly $10000 \text{ km} / N$
 - $2\pi R = 40000 \text{ km}$
 - 4 faces around circle
- Ratio between max and min cell width is $\sqrt{2} \approx 1.41$



c16 grid

$\Delta x \approx 625 \text{ km}$

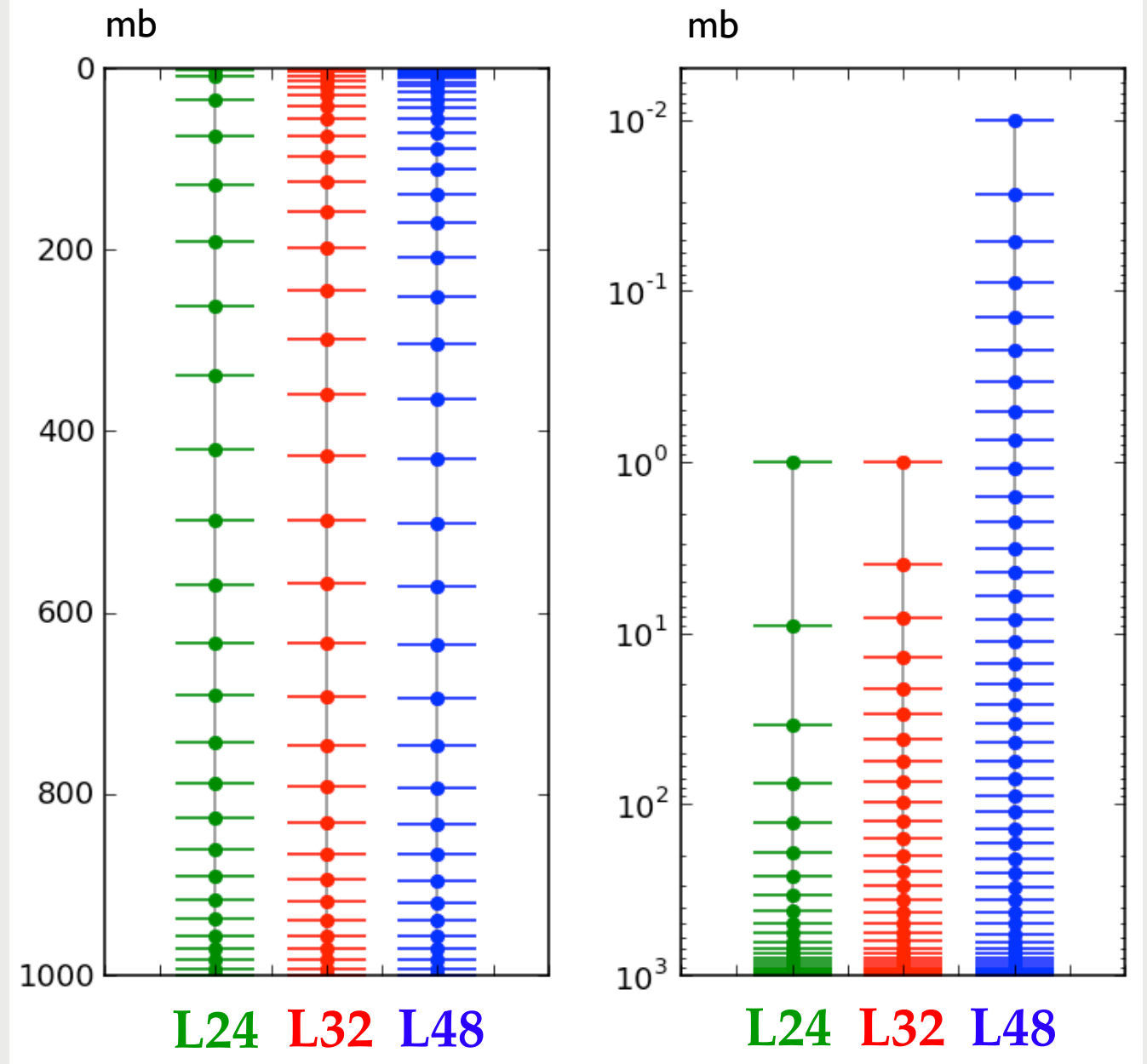
500 to 750 km

MODEL RESOLUTION

Grid	Avg. Δx	Equiv. $\Delta\Phi$
c16	625 km	5.5°
c48	210 km	2°
c90	110 km	1°
c180	55 km	0.5°
c360	25 km	0.25°
c720	12 km	0.125°
c2560	4 km	0.35° (2')

VERTICAL RESOLUTION

- npz: number of vertical layers
- AM2: 24
- AM3: 48
- HiRAM: 32
- Layer thicknesses are pre-defined for each npz



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  fill        = .true.
  print_freq  = 0,
  grid_type   = 0,
  old_divg_damp = .true.,
  nord        = 0,
  dddmp       = 0.0,
  d2_bg       = 0.0075,
  d4_bg       = 0.00,
  tau         = 0.

```

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dt_atmos = 1200
```

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/
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computing services

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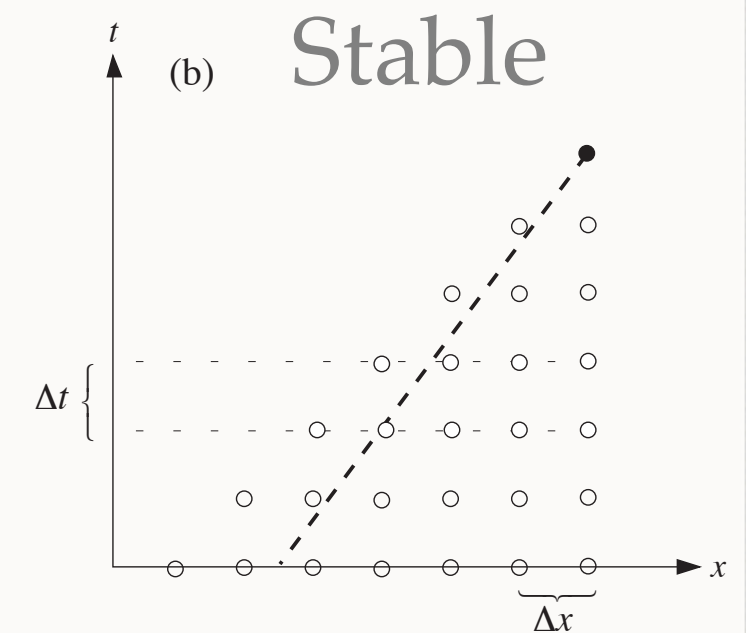
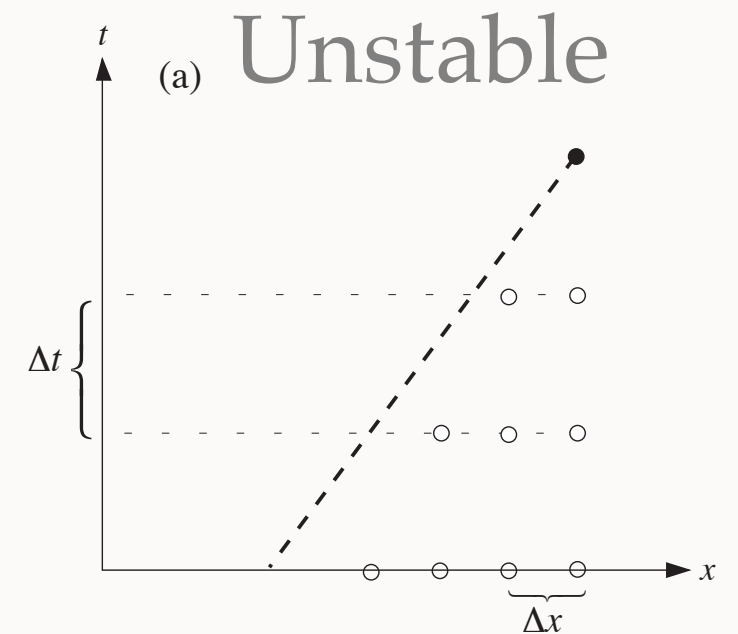
Dynamics

Diagnostics

Grid options

TIMESTEPS AND THE CFL RESTRICTION

- Courant number: $C = U\Delta t / \Delta x$
- Courant-Friedrichs-Lewy condition: stable only if signals in the exact PDE do not leave the numerical domain of dependence
- For the hydrostatic FV Core $C < 1$ is required



Durran, 2009

TIME STEPPING IN THE FV CORE

- `dt_atmos`: physics timestep (except radiation)
- `k_split`: number of vertical remappings per physics timestep
 - Usually 1 (default) or 2
- `n_split`: number of dynamical timesteps per `k_split` step
 - $\Delta t = dt_atmos / (k_split * n_split)$

CHOOSING YOUR TIMESTEP: N_SPLIT

- $n_split = dt_atmos / (\Delta t * k_split)$
- Ideally:
$$n_split = \lceil dt_atmos * U_{max} / (\Delta x_{min} * k_split) \rceil$$
- **However...**nonlinearity and gravity wave propagation require a smaller Courant number
- U_{max} can be quite large in the stratosphere!

A BEST FIRST GUESS

- Set `n_split = 0` to get an automatic guess from the model
 - Look in `stdout` for the selected `n_split`
- May need to tweak value anyway
 - If your model crashes, try increasing `n_split` first (**instead** of decreasing `dt_atmos`)

EXAMPLE #1: C48

- $\Delta x_{\text{avg}} = 210 \text{ km}$
- If $\text{dt_atmos} = 1200 \text{ s}$ and $\text{k_split} = 1$ (default):

```
starting          1  OpenMP threads per MPI-task
For k_split (remapping)= 1
n_split is set to 05 for resolution-dt=0049x0049x6- 1200.000
Using n_sponge : 00
Using non_ortho :      T
Starting PEs :      96
Starting Threads :      1
```

- $\Delta t = 1200 \text{ s} / 1 / 5 = 240 \text{ s}$
- $C \approx 200 \text{ m/s} * 240 \text{ s} / (210 \text{ km} * 0.8) \approx 0.29$

EXAMPLE #2: C720

- $\Delta x_{\text{avg}} = 12 \text{ km}$
- If $\text{dt_atmos} = 300 \text{ s}$ and $\text{k_split} = 2$:

```
starting          1  OpenMP threads per MPI-task
For k_split (remapping)=          2
n_split is set to 09 for resolution-dt=0721x0721x6- 300.000
Using n_sponge : 00
Using non_ortho :      T
Starting PEs :          96
Starting Threads :          1
```

- $\Delta t = 300 \text{ s} / 2 / 9 = 17 \text{ s}$
- $C \approx 200 \text{ m/s} * 17 \text{ s} / (12 \text{ km} * 0.8) \approx 0.35$

TRACER SUB-CYCLING

- Tracers are advanced **after** completing n_split dynamical timesteps using the accumulated air mass fluxes
- Since tracer advection is linear and depends only on the wind speed, the Courant number can be closer to 1.
- By default ($q_split = 0$) the model computes the number of split tracer timesteps automatically:
 - $\max \{ \sum_{n_split} C \} + 1$

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  npz         = 48,
  n_split     = 8,
  a2b_ord     = 4,
  adjust_dry_mass = $adjust_dry_mass,
  consv_te    = 0.7,
  fill        = .true.
  print_freq  = 0,
  grid_type   = 0,
  old_divg_damp = .true.,
  nord        = 0,
  dddmp       = 0.0,
  d2_bg       = 0.0075,
  d4_bg       = 0.00,
  tau         = 0.
/

&coupler_nml
  ...
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/

```

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DIVERGENCE DAMPING

- One of two means of noise control in FV Core
- `nord`: order of divergence damping
 - `nord = 0` : ∇^2 divergence damping
 - `d2_bg`: damping coefficient, default 0
 - `nord = 1`: ∇^4 divergence damping; more scale selective (default)
 - `d4_bg`: damping coefficient, default 0.16, maximum 0.25

UPPER SPONGE LAYER

- Top two layers are wave-absorbing layers, implemented through additional divergence damping and diffusive lower-order flux operators
 - `old_divg_damp = .true.` : From CMIP5 runs
 - `n_sponge = 0:2` layers with presets good for high-resolution simulations
 - (must have `old_divg_damp = .false.`)
 - `n_sponge = 1:2` sponge layers (default)
 - `n_sponge > 1: n_sponge + 1` sponge layers

OTHER DAMPING PARAMETERS

- `tau`: strength of Rayleigh friction applied near top boundary; 0 by default
- `d_ext`: barotropic (“external”) mode damping; 0.02 by default, maximum 0.25
- `d_con`: rate at which energy dissipated by divergence damping turned into heat, so as to better conserve energy. 0 by default; use at your own risk

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TRACER FILLING

- Positive-definite Lin & Rood tracer advection produces tiny negatives (10^{-25} and smaller)
- Set `fill = .true.` when it absolutely, positively **must** be positive
- Negative filling is done in the **vertical** to avoid possibly having to reach across process domains

CONDENSATE LOADING

- The FV core uses the microphysical tracers to *explicitly* compute condensate loading of `nwat` species
 - `nwat` = 3 by default, for three-phase AM3 microphysics
 - If using six-phase Lin microphysics set `nwat` = 6
 - Don't want loading? Set `nwat` = 0

DYNAMICS PARAMETERS

- `beta`: time-centering parameter for pressure-gradient force
 - 0 by default; 0.4 may improve solution of gravity waves in the tropics
- `hord_tr`: tracer advection scheme
 - 12 by default: monotone and positive-definite
 - 13: positive-definite only, faster

DYNAMICS PARAMETERS

- `a2b_ord`: order of interpolation of pressure to corners for PGF; 4 by default
- `consv_te`: amount to correct total energy lost in dynamics and vertical remapping
 - 0 by default; 0.7 in full-physics simulations


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  adjust_dry_mass = $adjust_dry_mass,
  consv_te    = 0.7,
  fill        = .true.
  print_freq  = 0,
  grid_type   = 0,
  old_divg_damp = .true.,
  nord        = 0,
  dddmp       = 0.0,
  d2_bg       = 0.0075,
  d4_bg       = 0.00,
  tau         = 0.
/

&coupler_nml
  ...
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/

```

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PRINT_FREQ

```

      1      0
ZS max = 0.0000000000000000E+000 min = 0.0000000000000000E+000
PS max = 1015.000000000000 min = 1004.82291130741
Mean specific humidity (mg/kg) above 75 mb= 9.999999999999999E-006
Total surface pressure (mb) = 1014.99347525107
mean dry surface pressure = 1010.06551436790
Total Water Vapor (kg/m**2) = 50.2853151343074
ENG Deficit (W/m**2)= 0.0000000E+00
UA max = 19.1862477411642 min = -19.5545697489168
VA max = 19.6695572008257 min = -19.2094634974794
TA max = 301.987126680501 min = 201.007851200000
OM max = 0.0000000000000000E+000 min = 0.0000000000000000E+000
RH_sf (%) max = 84.1964443194992 min = 83.1611373517436
RH_3D (%) max = 84.1964443194992 min = 1.838996873108497E-006
PoTemp max = 1178.99543758473 min = 301.006081741117
sphum max = 2.075856765343869E-002 min = 9.999999999999999E-012
```

- Hours between diagnostic printout
 - 0 (default) for no output
 - Set to -1 to get output every timestep

DEBUGGING OUTPUT

- `fv_debug = .true.` prints out max/min at beginning and end of every call to the FV core
- `range_warn = .true.` prints warnings if model variables exceed reasonable bounds
- Both are `.false.` by default
- Any diagnostic output will slow down the model

INITIAL CONDITIONS

- Set `external_ic = .true.` to use external lat-lon data source given in `res_latlon_dynamics`
- When initializing the model, set `adjust_dry_mass = .true.` to add the mass of water vapor to the initial mass to account for condensate loading
 - Automatically set in most scripts

INITIAL CONDITIONS

- When `external_ic = .true.:`
- `ncep_ic = .true.` if using an NCEP or NCEP-compatible analysis or reanalysis
- `diag_ic = .true.` if instead using a lat-lon FV core output file
- Can also use `res_latlon_tracers` to initialize tracers with this option

BOUNDARY CONDITIONS

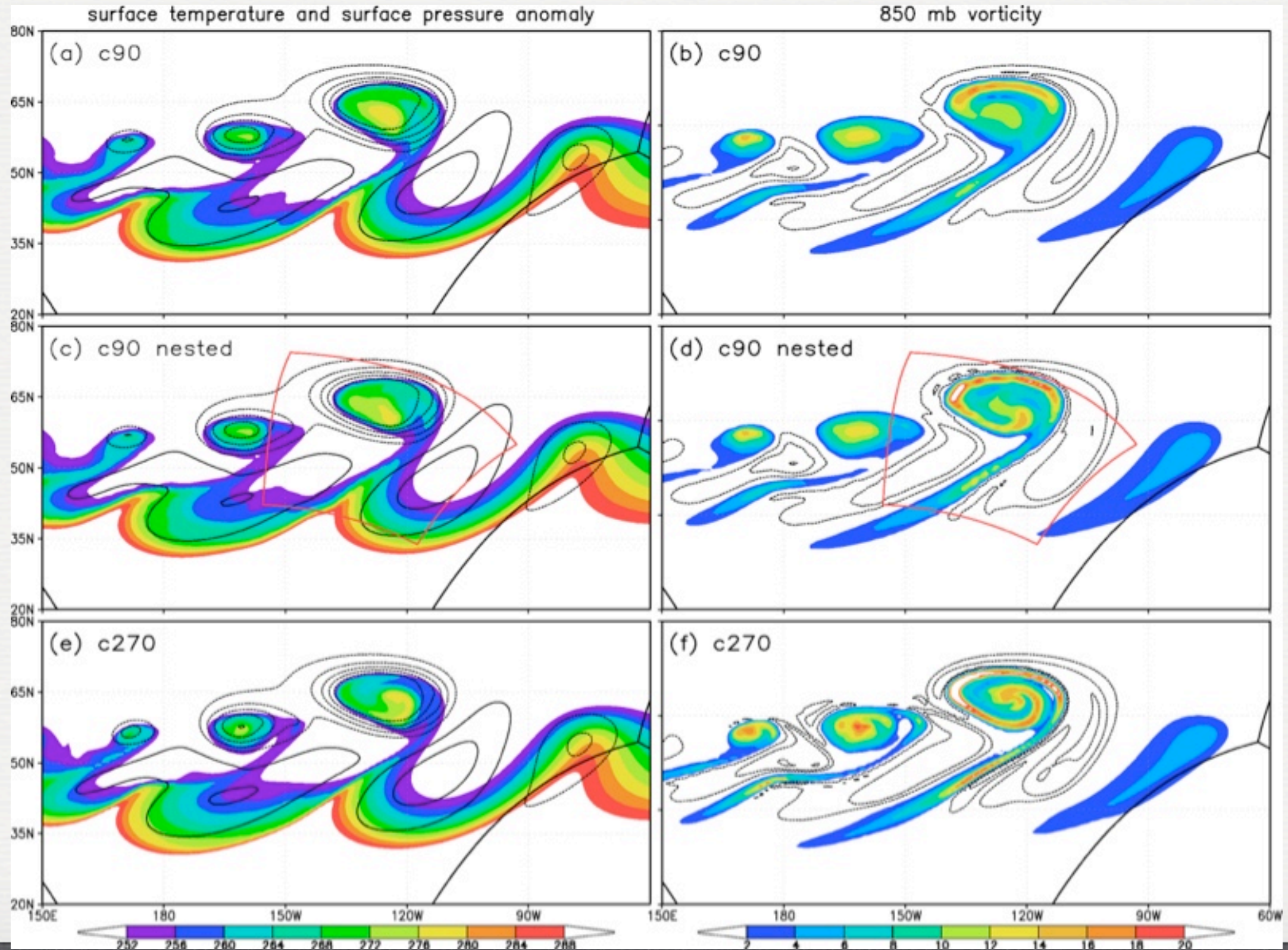
- Topography for FV core (and gravity wave drag) specified in `surf_map_nml`
- Specifying SSTs is done in `ocean_model_nml` and `amip_interp_nml`
- `nudge = .true.` uses input data in `res_latlon_dynamics` to nudge the solution to the analysis state

REFINED GRIDS: PRELIMINARY RESULTS

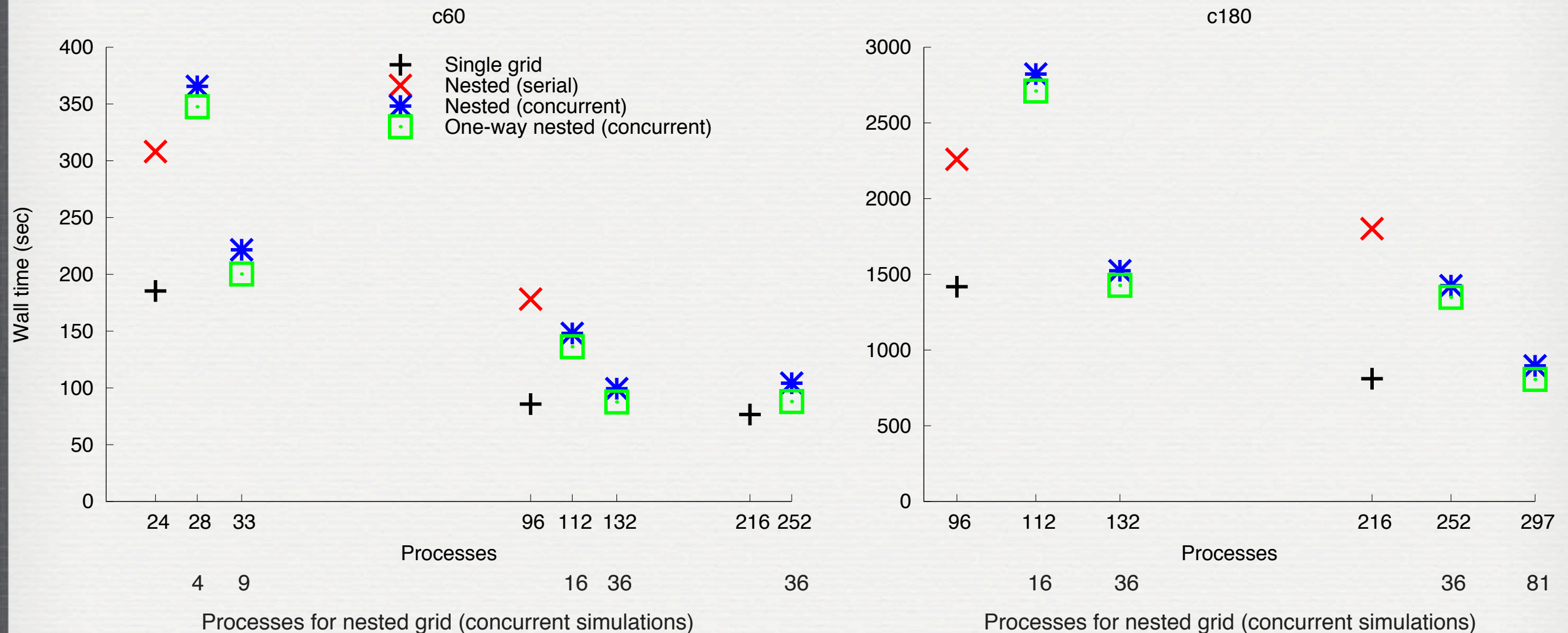
NESTED GRID

- Inserts a small, higher-resolution nested grid in global grid, with optional two-way feedback
 - Available in FV core
 - ✓ Flexible sizes, numbers
 - ✗ Conservation is much harder
 - ✗ Grid artifacts can be a problem

BAROCLINIC INSTABILITY TEST



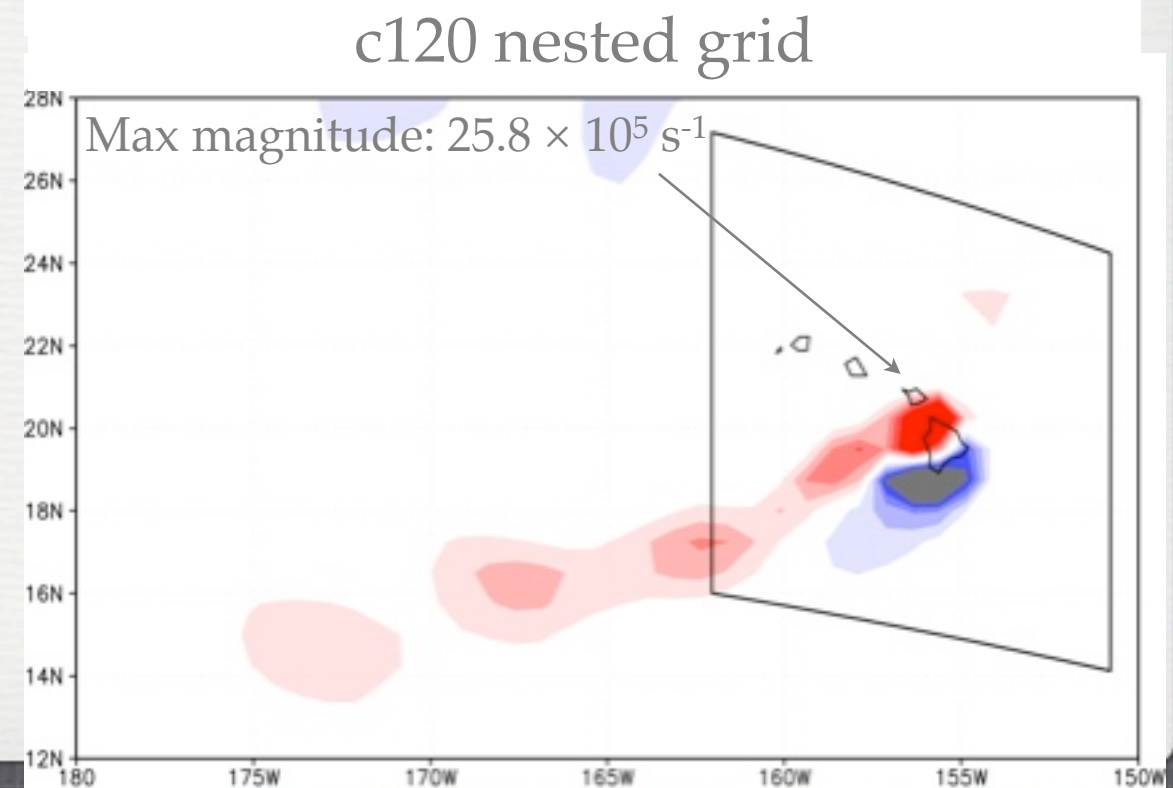
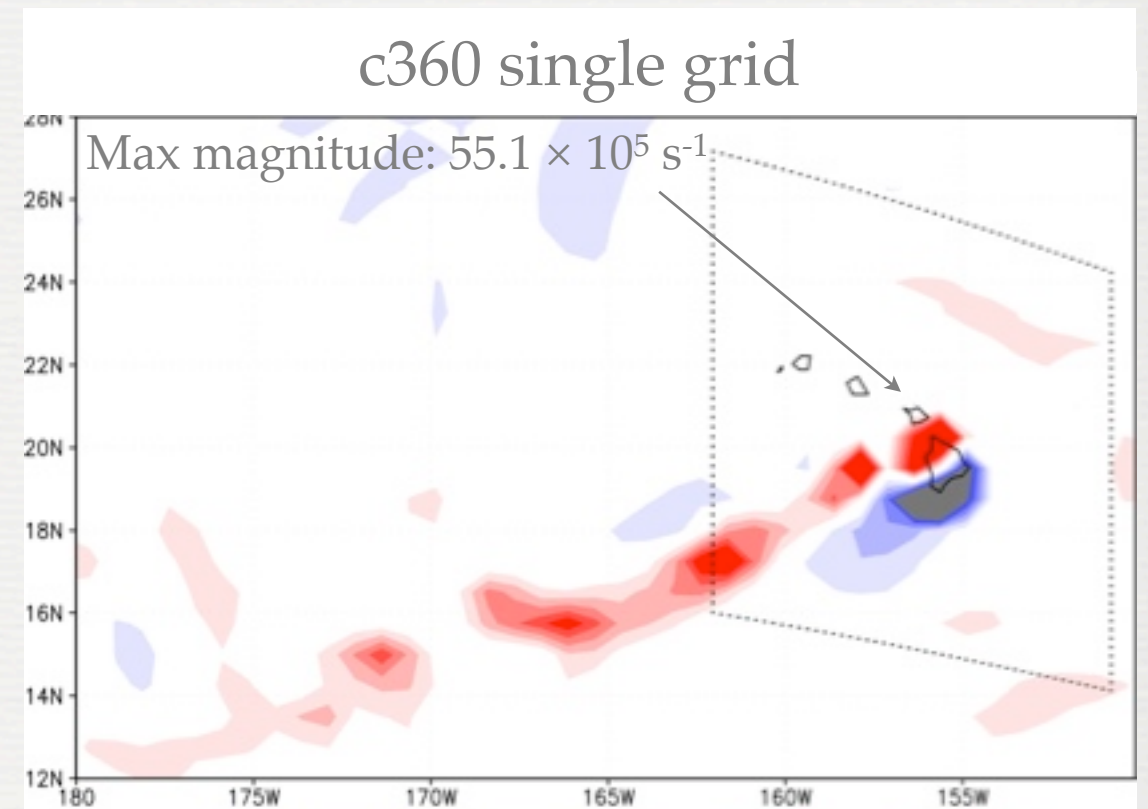
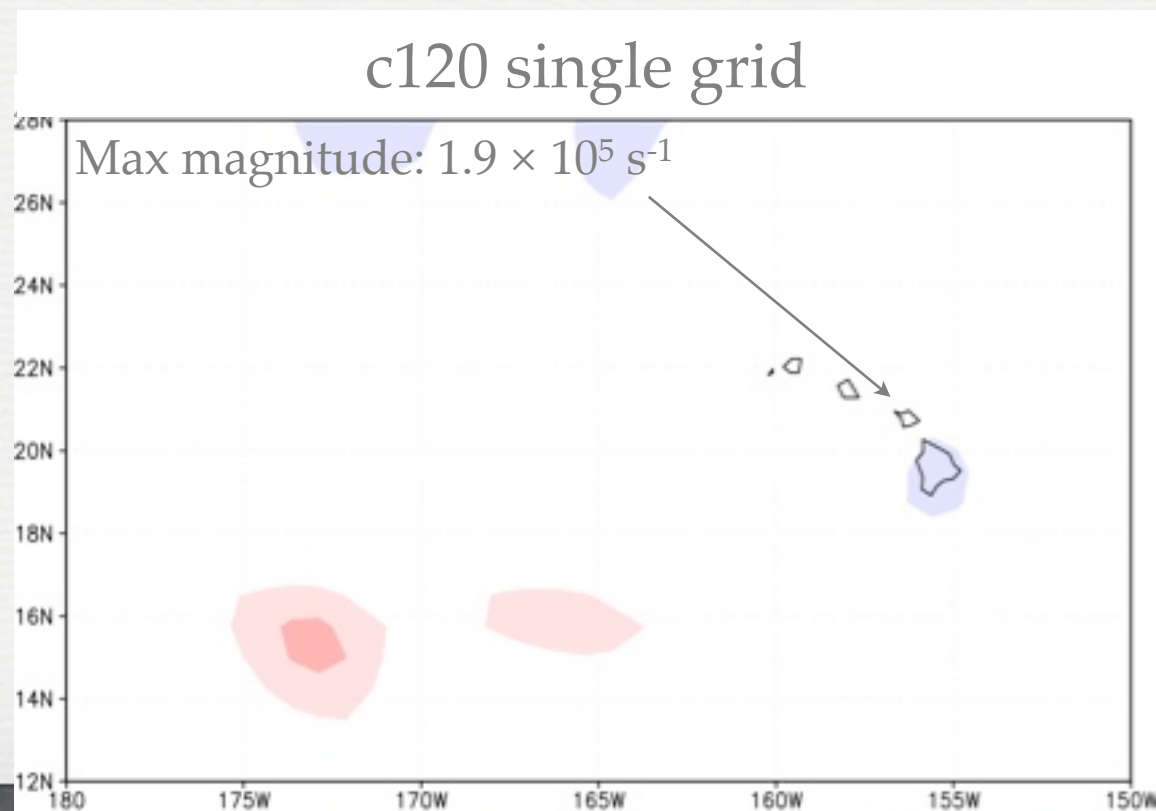
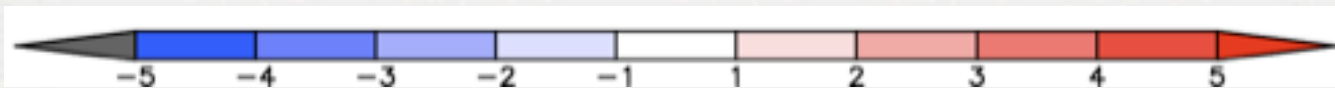
BC TEST: TIMING



- In an environment with many available processors, using additional processors for concurrent nesting can yield large efficiency gains!

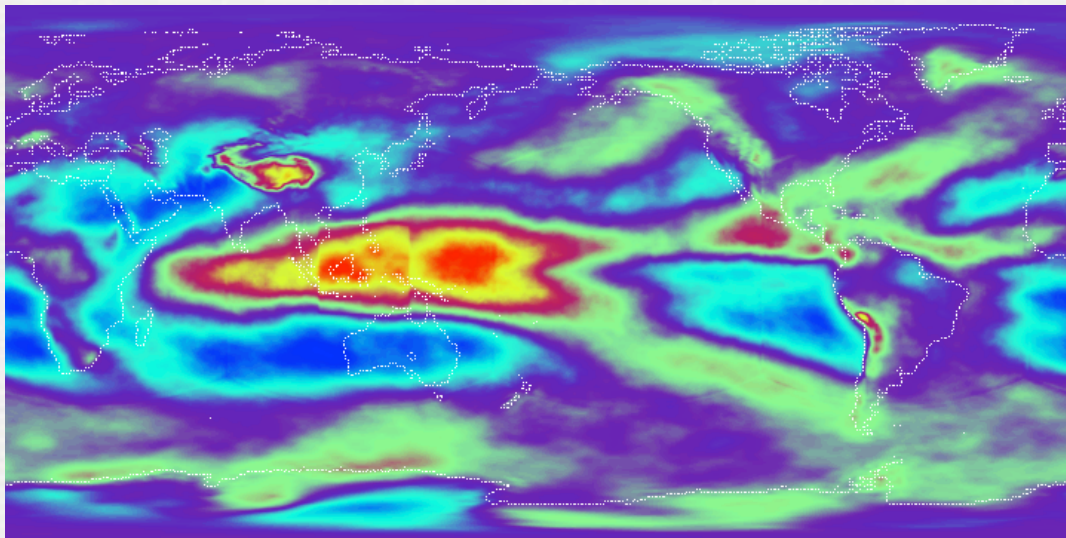
HAWAII LEE VORTICES

- 72 hr forecast from 1 Aug 2010 00Z with real topography
- Showing Vorticity $\times 10^5 \text{ s}^{-1}$, topping out at ± 5

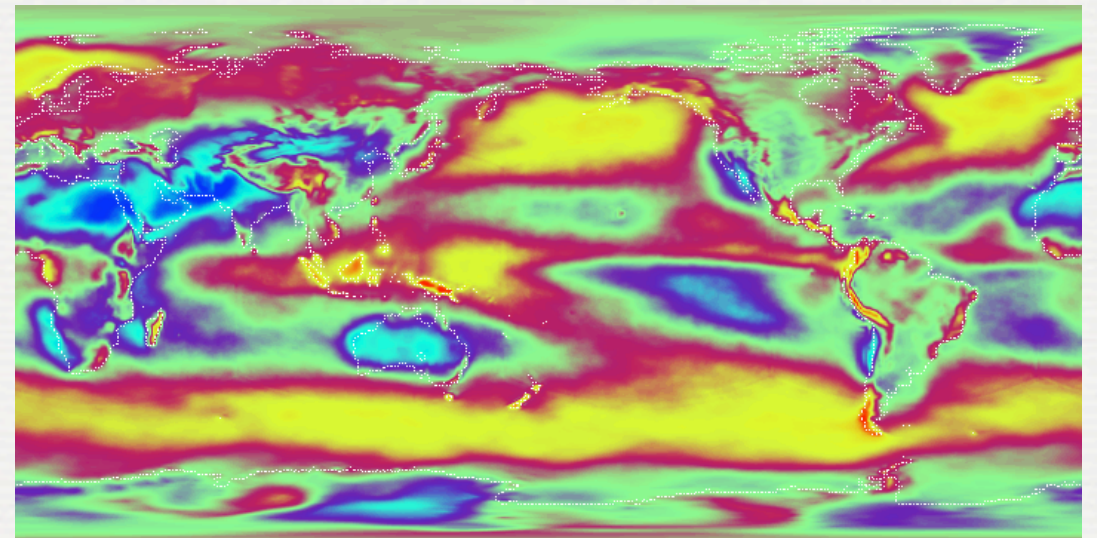


MARITIME CONTINENT C90 NESTED GRID

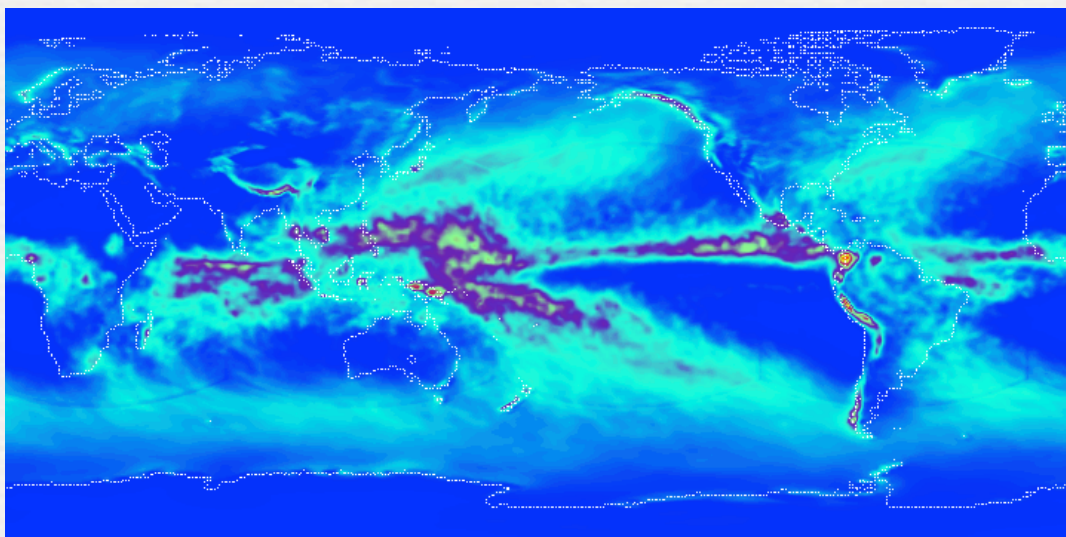
High cloud amount



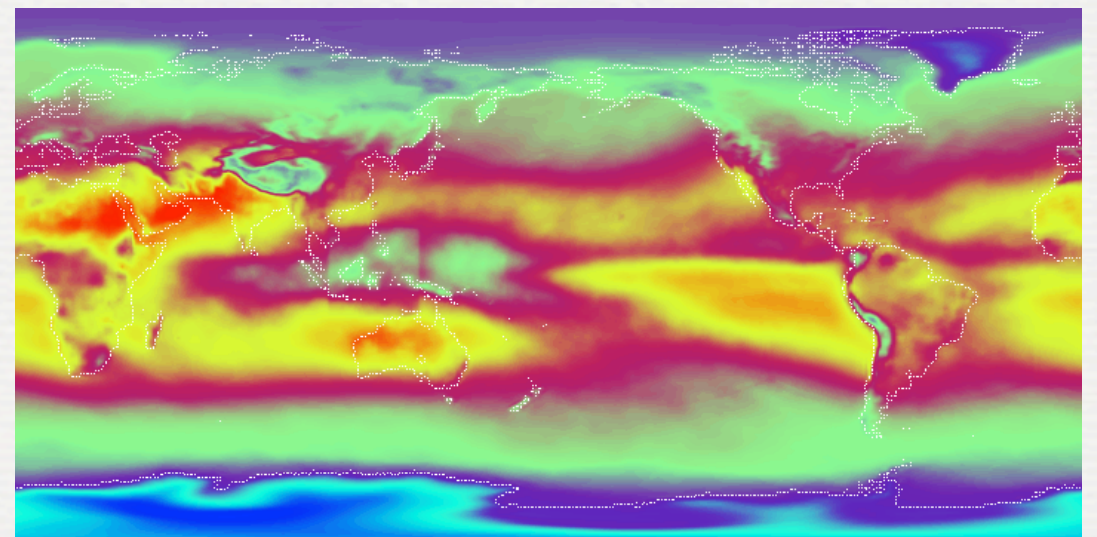
Total cloud amount



Precipitation

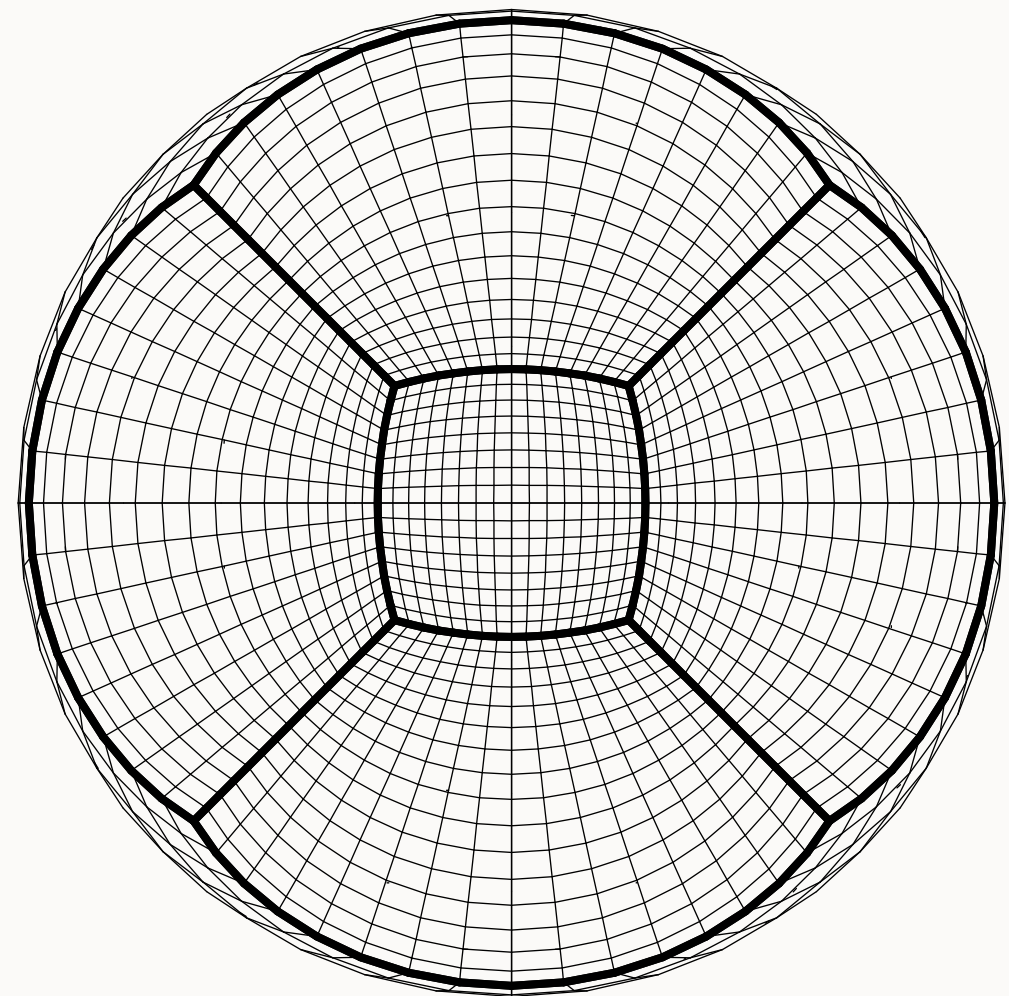


OLR



STRETCHED GRID

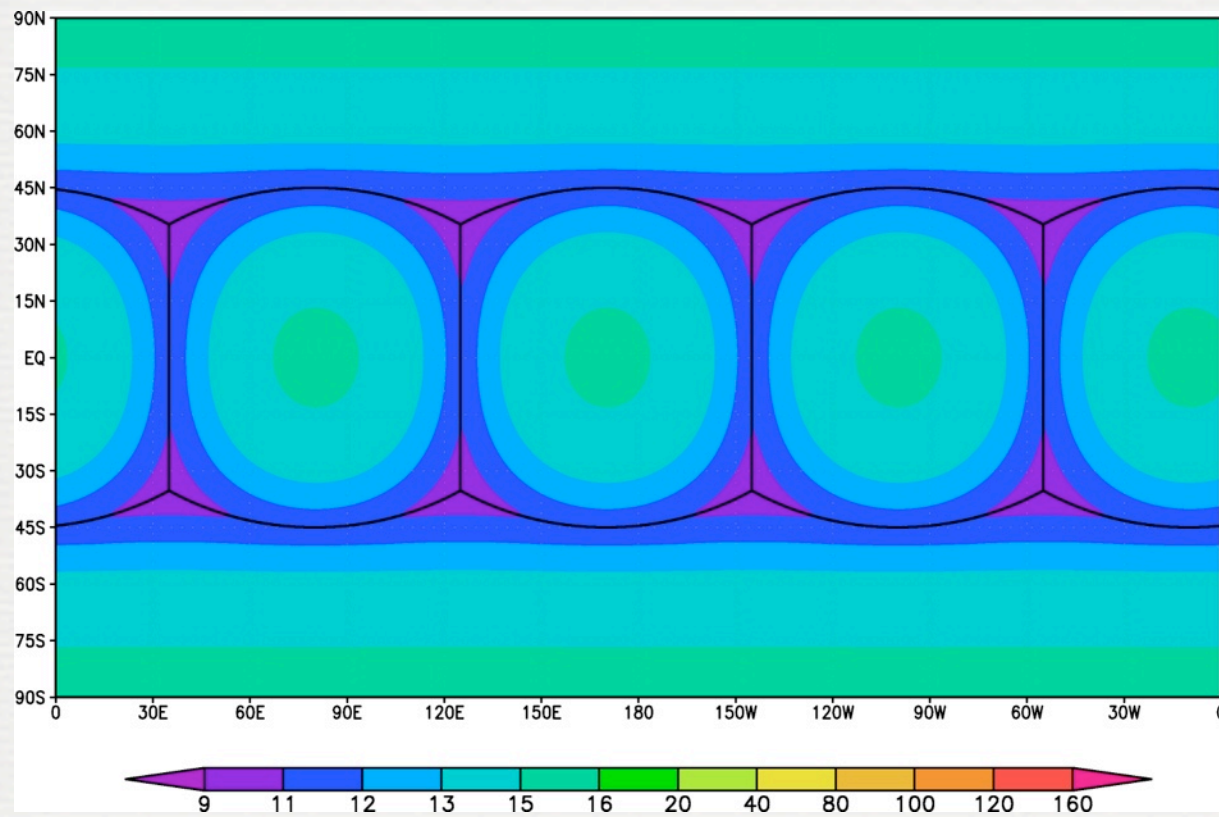
- Deforms cube into a truncated pyramid with one smaller face
 - Already in FV core
 - ✓ Slightly smoother than original cubed sphere
 - ✓ Automatically mass-conserving
 - ✗ Can only refine in one spot
 - ✗ Rest of solution degraded
 - ✗ Timestep restricted everywhere by smallest cell



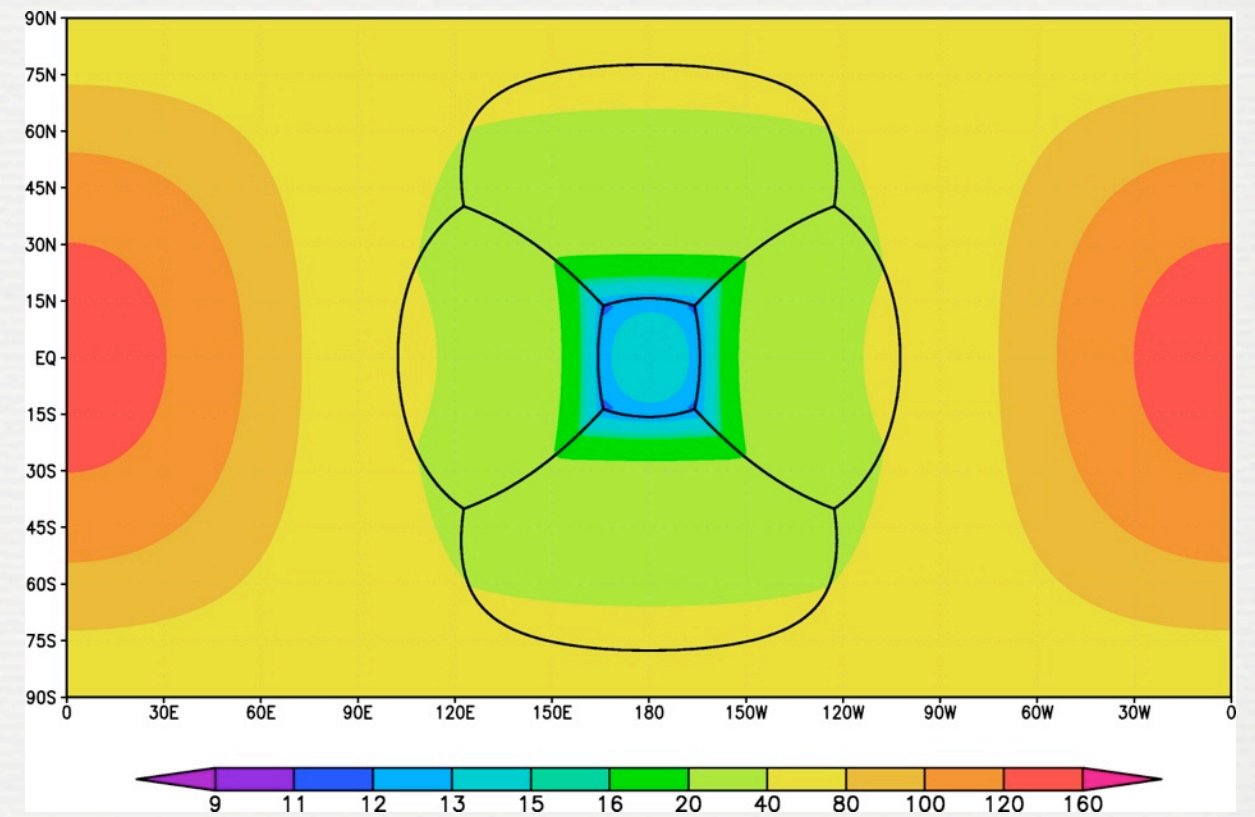
c16r3

$$\Delta x_{\text{avg}} = 625 \text{ km}$$

c720

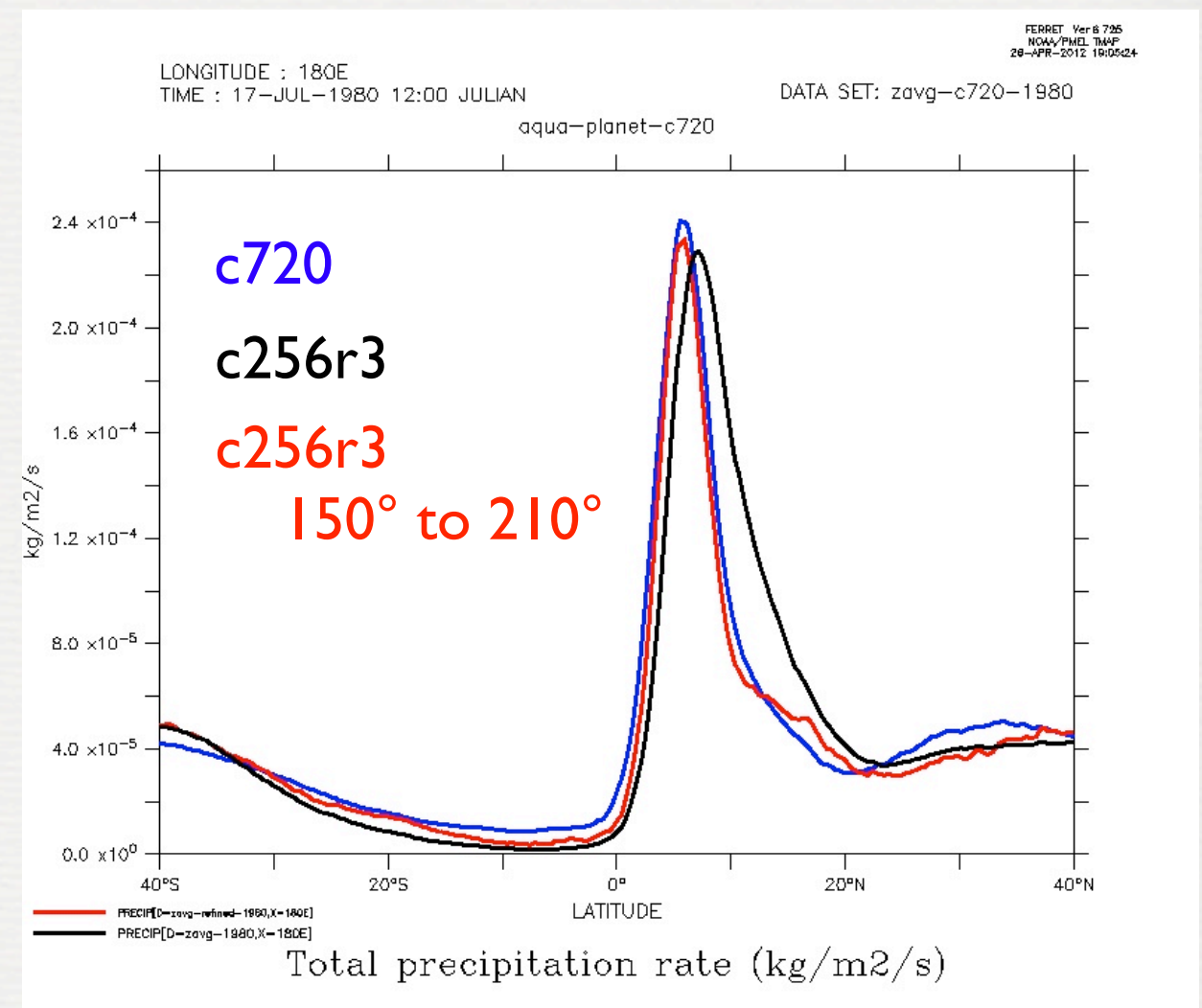
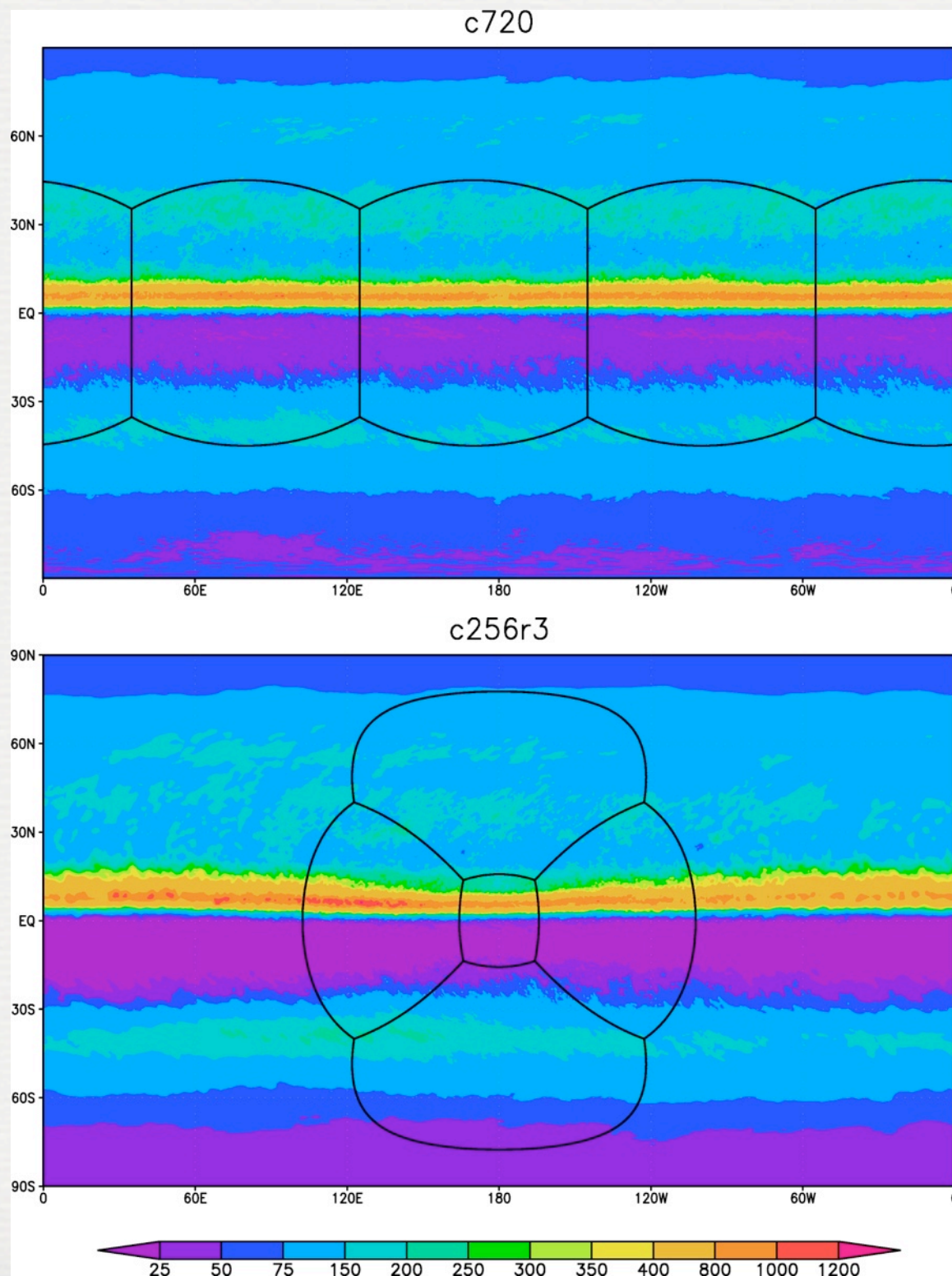


c256r3



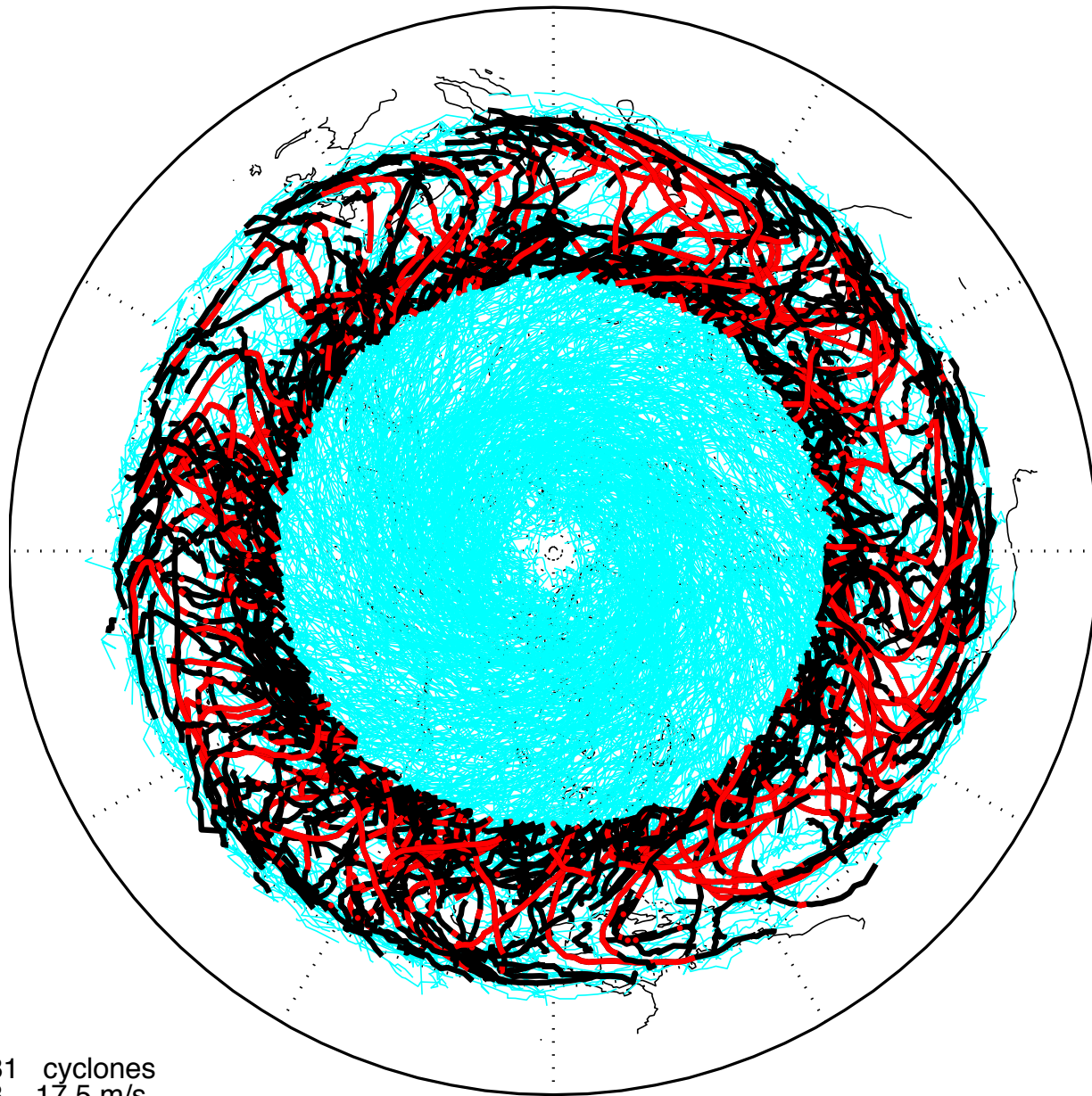
	c720	c256r3
Δx avg	12.9 km	~ 40 km
Δx min	10.9 km	~ 13 km
Δx max	15.4 km	~ 117 km

AQUAPLANET: PRECIPITATION



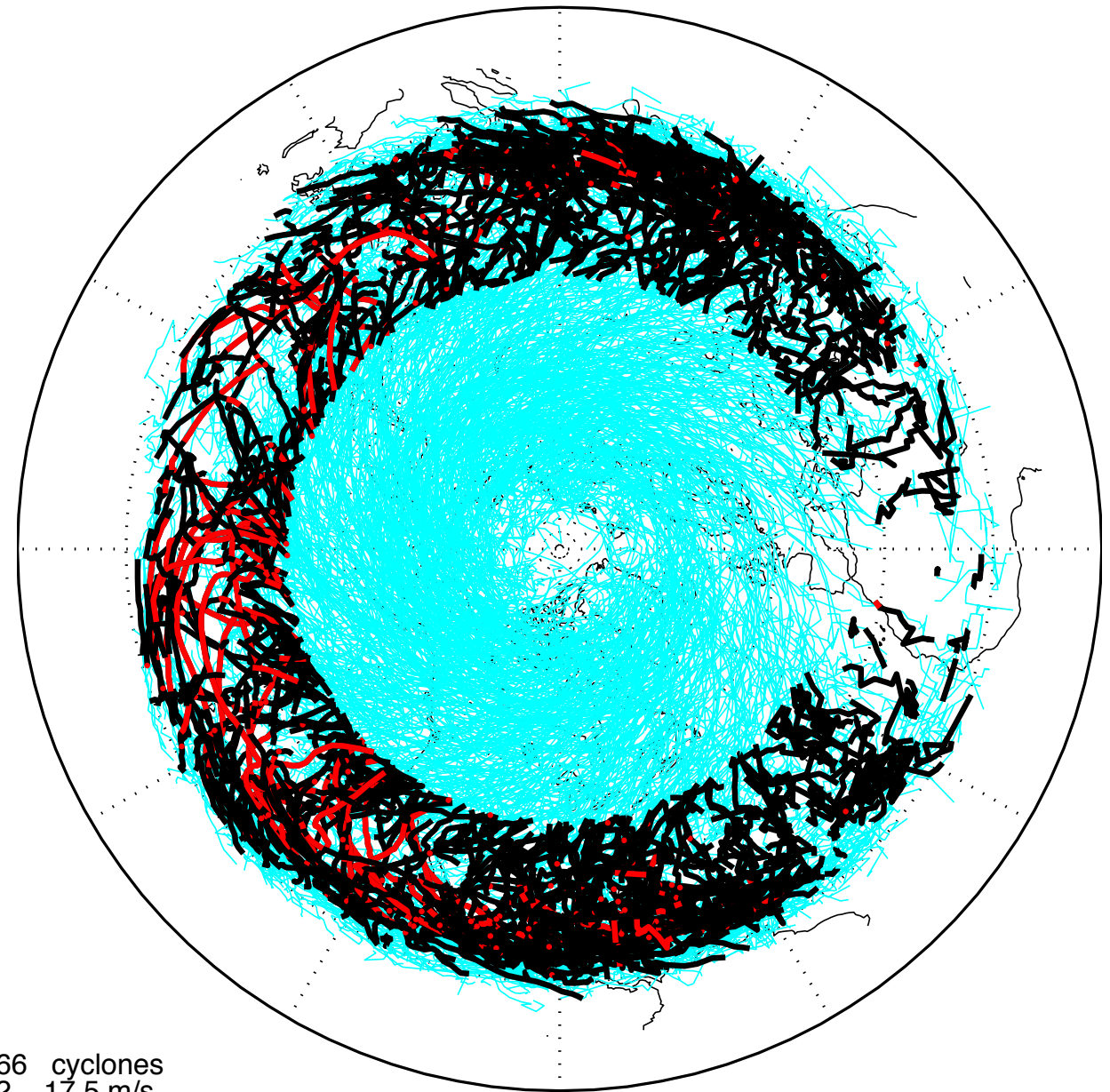
AQUAPLANET: TROPICAL CYCLONES

c720



2681 cyclones
513 17.5 m/s
263 32.5 m/s

c256r3



2866 cyclones
722 17.5 m/s
206 32.5 m/s